
„Hydroforming of Titanium Tubes“

Development of a multi stage hydroforming process for titanium tubes

Hannover Messe | Hanover | April, 12th, 2013



Context

- Hydroforming is a cost effective way of shaping metals into lightweight and strong pieces
- Titanium has a high potential for lightweight constructions
- Due to its low proportional elongation titanium was not processed by hydroforming yet

Intention

- Developing a hydroforming process for shaping titanium tubes

Result

- cost-efficient and complex lightweight parts with unprecedented properties

Overall Objective

- Developing a cost effective **process chain** for hydroforming **titanium tubes**

Subtasks

- Subtask 1: Analyzing **material properties** of several titanium alloys and their hydroforming **process limits**
- Subtask 2: Investigating adequate **heat treatments to reestablish the formability** for several alloys and forming processes
- Subtask 3: Ascertain a suitable **lubricant**

Scheduled Workflow

- Pre-distension, heat treatment and **tensile test** as well as microstructure analysis of metal strips (UTS, PA)
- Boundless expansion, heat treatment and **burst testing** tube (UTS, PA)
- **Tribological examinations** (IPH, PA)
- **Process verification** on a demonstration part (IPH, if necessary PA)



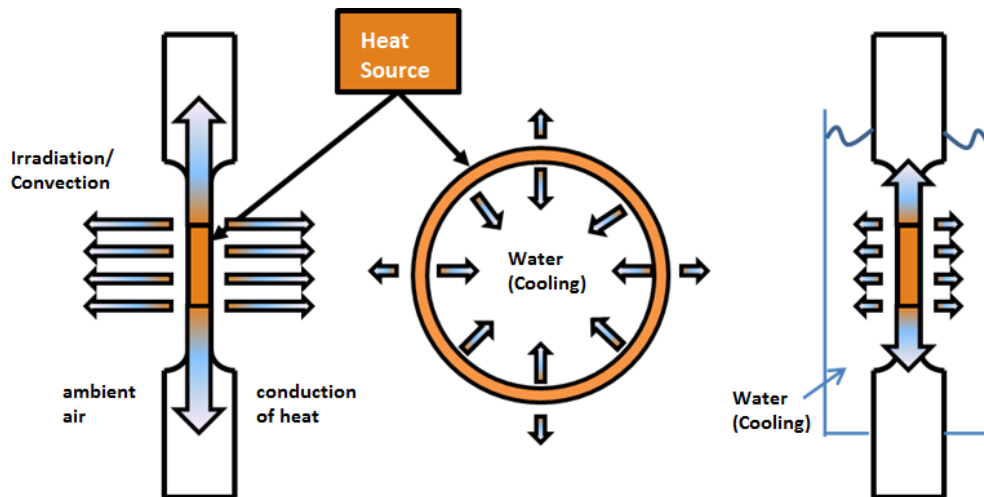
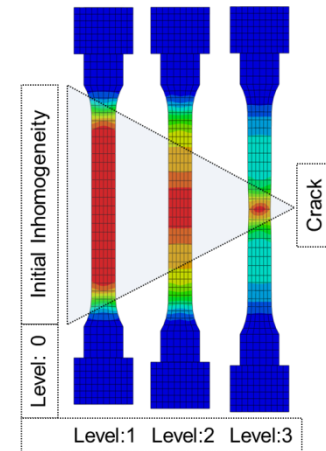
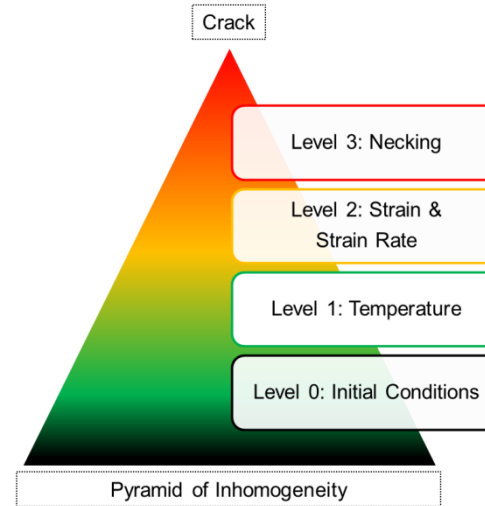
Expected Results

- Selection of a suitable **heat treatment**
- Analyze the **influence of the tube production** on the workability of titanium alloys
- Ascertain suitable **lubricants**
- Final outcome: **Guidelines for hydroforming titanium tubes**

Assimilation of tensile strength test

Pyramid of Inhomogeneity

→ Isothermal tensile test

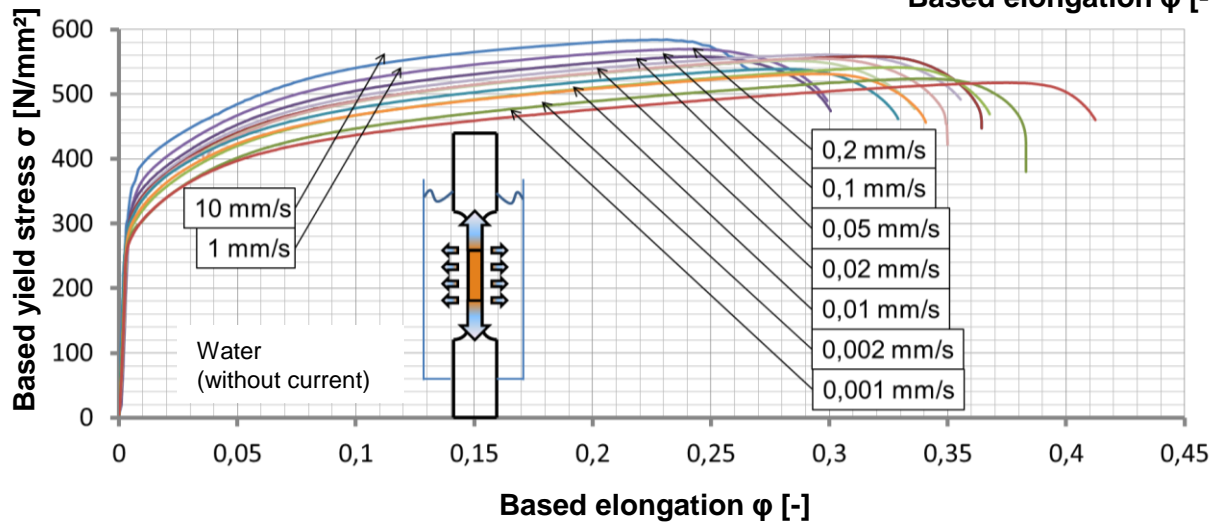
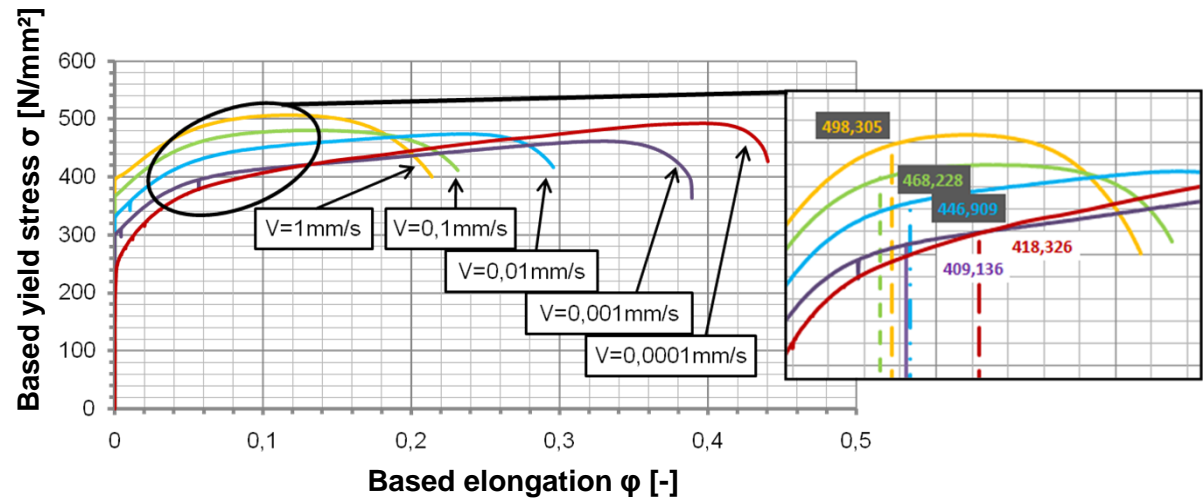


Cooling Influence

Common tensile test

Isothermal tensile test

→ Isothermal tensile test



Mathematical description

— Nadai's approach:

$$k_f(T, v) = A(T, v) * \varphi_v^{n(T)}$$

$$k_f(T, v) = \begin{cases} v = [0,001 - 10] \text{ mm/s} \\ T = [20 - 80]^\circ \text{ C} \end{cases}$$

$$A(T, v) = A_{Start} + \ln\left(\frac{V}{V_{ref}}\right) \left(0,0077\left(\frac{T}{T_{ref}}\right) + 20,804\right) - 1,7581\left(\frac{T}{T_{ref}}\right)$$

$$n(T) = n_{start} - 0,00007\left(\frac{T}{T_{ref}}\right)$$

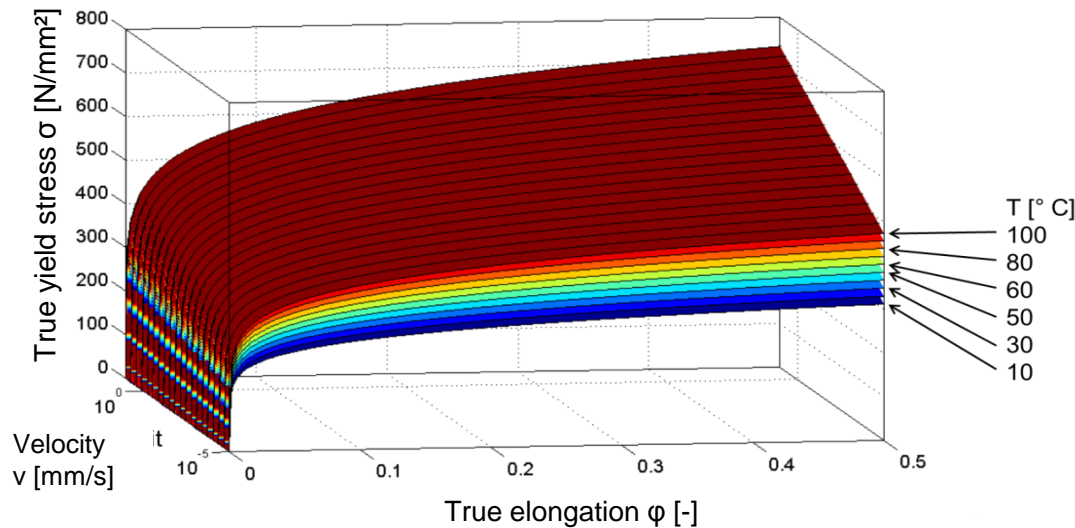


Illustration of a multi-stage process chain with sheet specimens

— tensile test with optimized heat treatment parameters:

- Pre-distension: $\epsilon_{pre} = 15 \%$, ($\epsilon_{min} = 5 \%$)
- Annealing temperature: $T_{heat} = 750^\circ \text{C}$
- Annealing time: $t_{heat} = 20 \text{ min}$
- Cooling: $k = 750^\circ \text{C} / 5 \text{ h}$

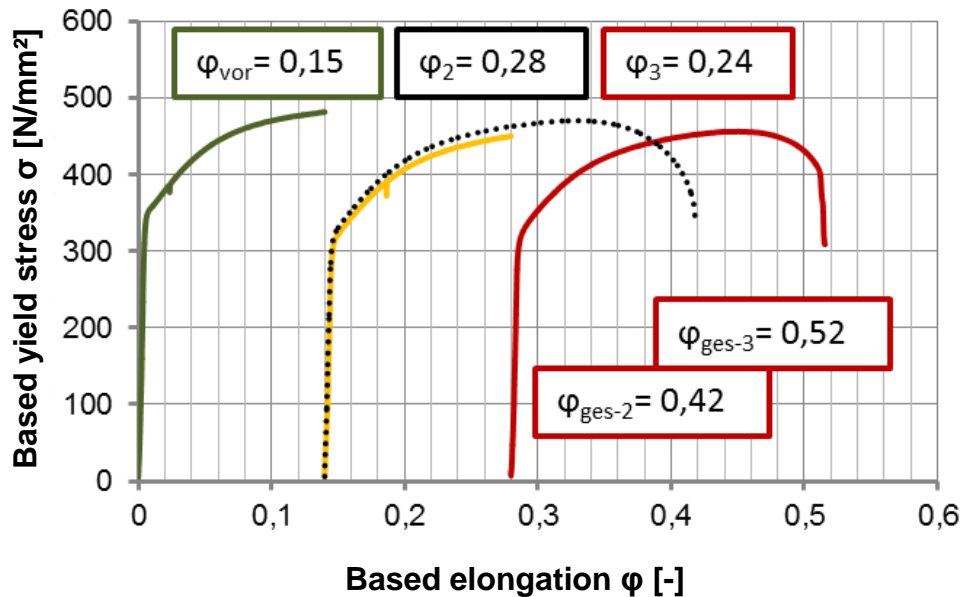
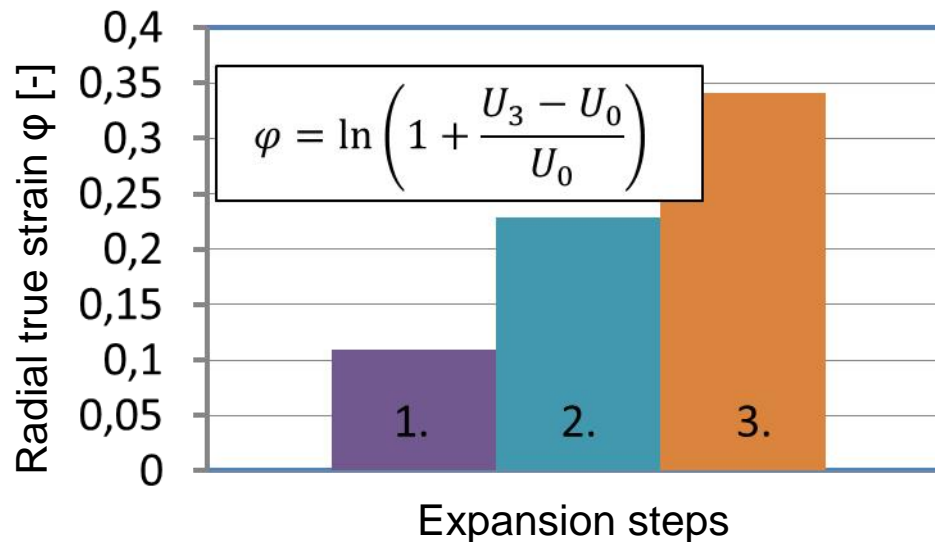


Illustration of a multi-stage process chain with tubes

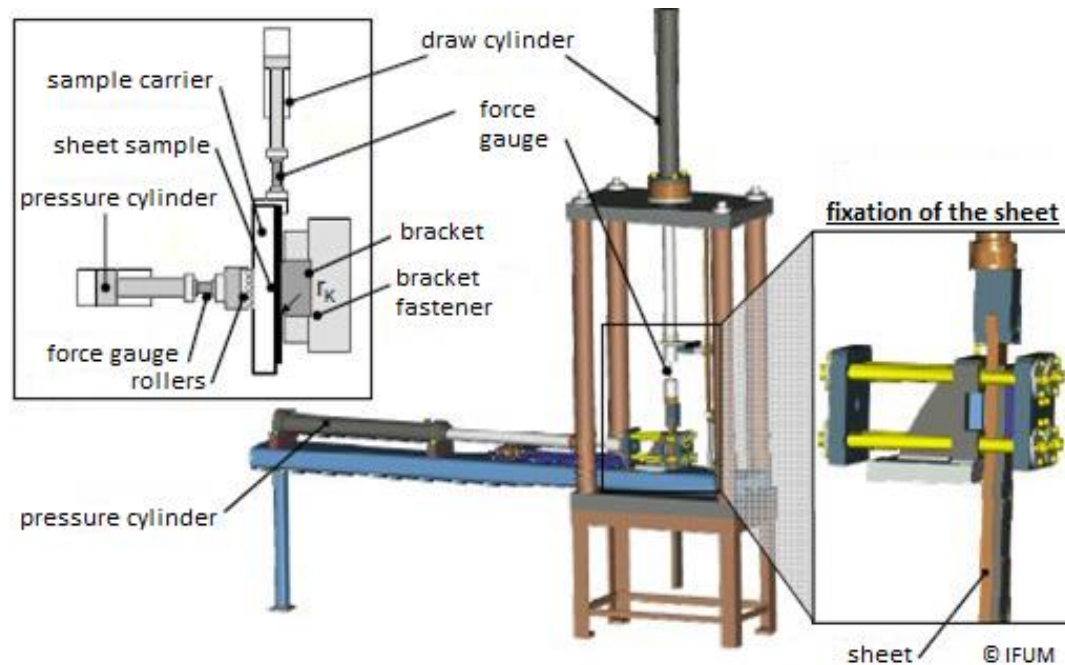
— Burst test with free ends

- Pre-distension: $\epsilon_{pre} = 12 \%$, ($\epsilon_{min} = 5 \%$)
- After the third forming stage there was a maximum strain of $\varphi = 0,35$



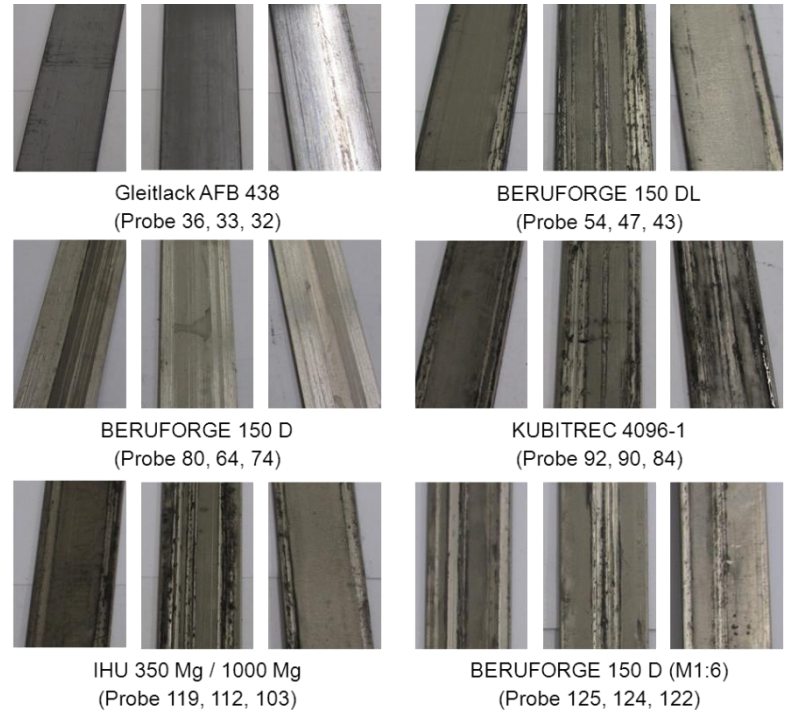
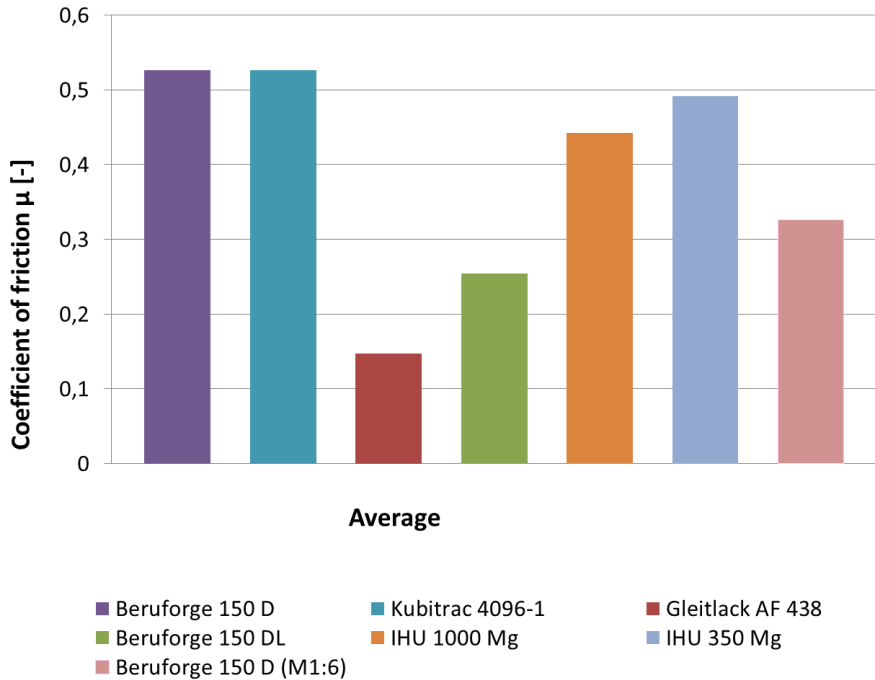
Provided lubricants

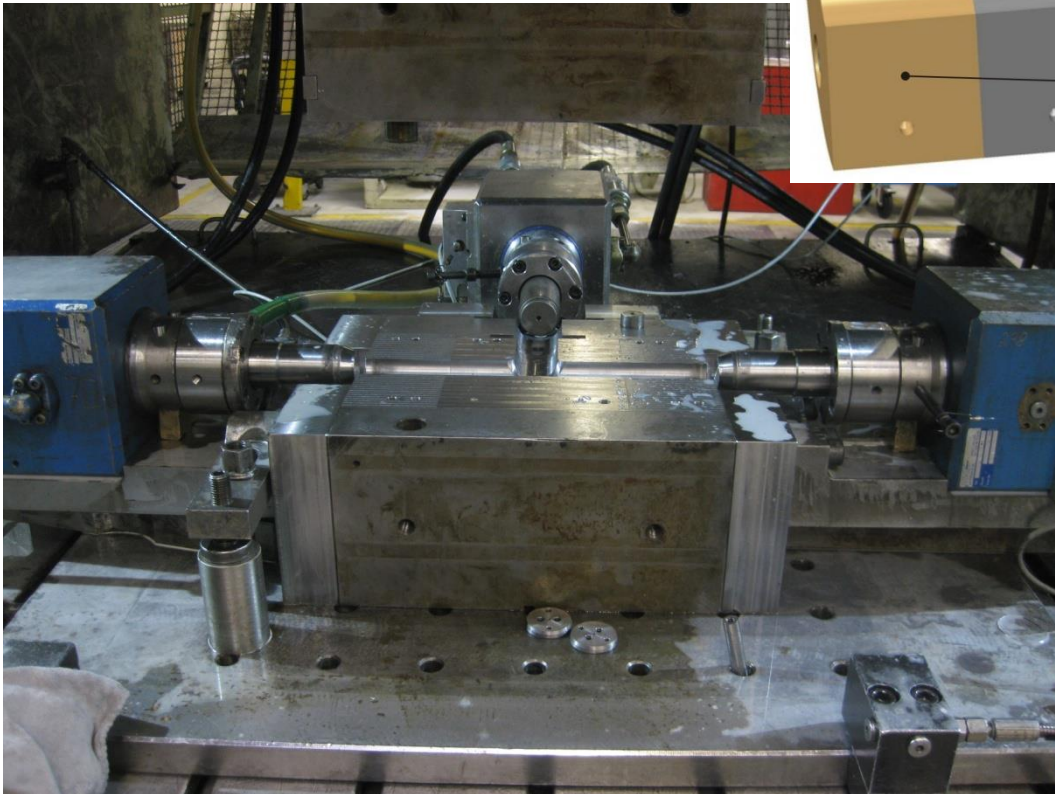
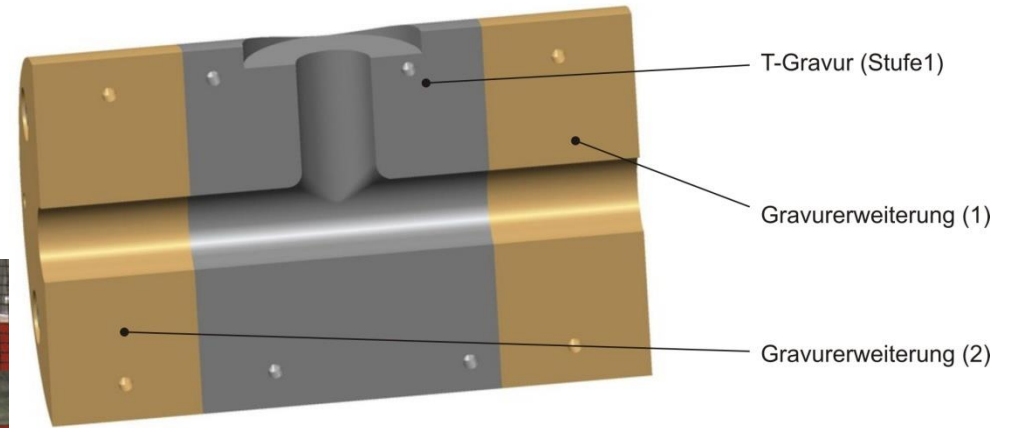
- Berucoat AF 438 (air-hardening inorganic MoS₂/Graphite – sliding lacquer) [B]
- Beruforge 150 DL (water-soluble drawing paste) [B]
- Beruforge 150 D (water-soluble drawing paste) [B]
- Kubibrac 4096-1 (fully synthetic high performance drawing oil) [B]
- Raziol IHU 350 Mg [R]
- Raziol IHU 1000 Mg [R]



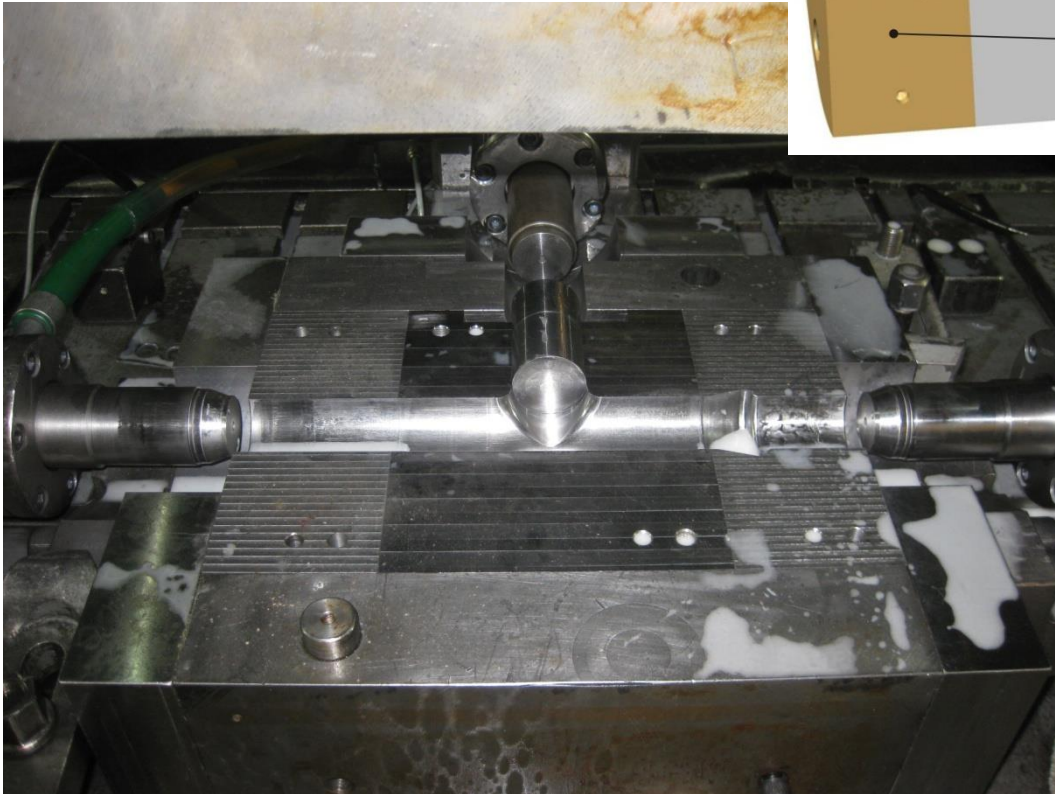
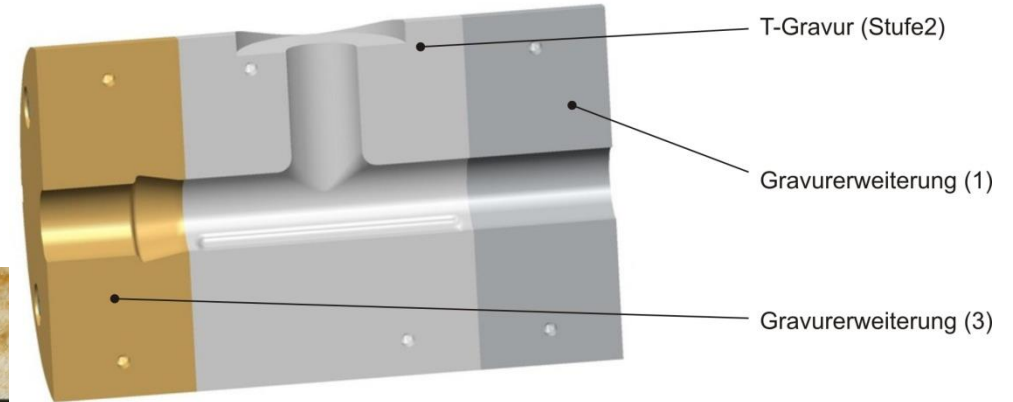
Results of the strip drawing test

Coefficient of friction dependent on several laminations





Dies of the Second Forming Stage





Sample 44	Stage 1	Stage 2
(Strut-) Height	62,52 (~23 %)	70,56 (~38,9 % [~12,9 %])
Length	341,5	319
Circumference	199	214
Diameter	~ 51	51,09

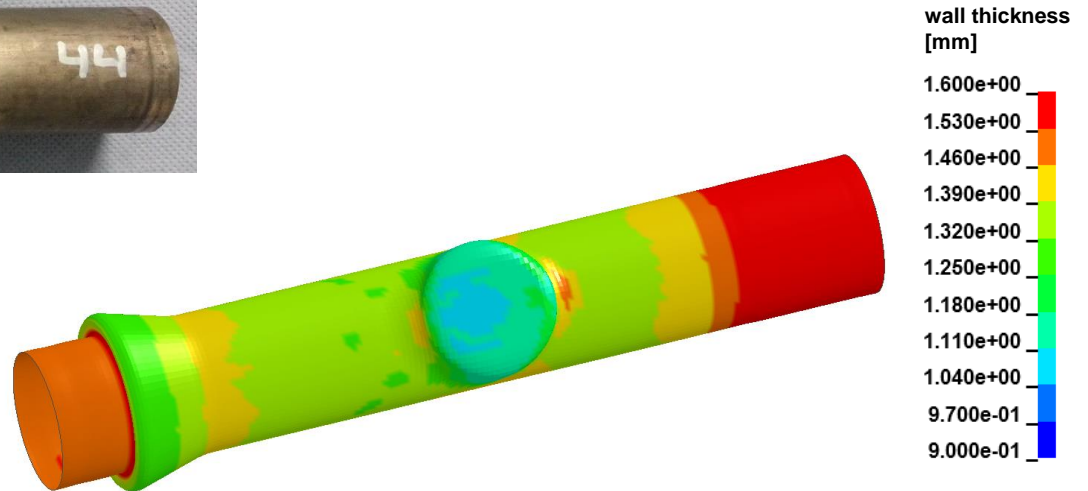
Sample 44

— Stage 1

Time [s]	0,2	2	4	10,6	11,6	12,6
Pressure [bar]	180	250	330	380	390	585 (620)
Punch 1&2 [mm]	0,3	1,7	8	15	17	26 (27)
Strut [mm]	0	0	0	5	7	1

— Stage 2

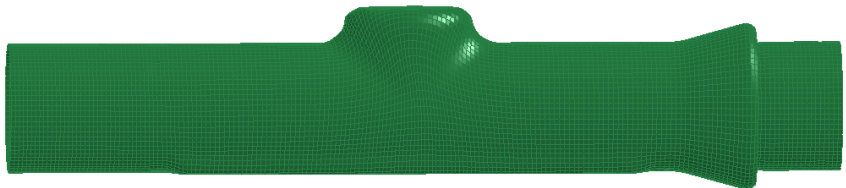
Time [s]	0,2	2	4	10,6	11,6	12,6
Pressure [bar]	180	250	330	380	390	620
Punch 1 [mm]	0,3	1,7	8	15	17	22
Punch 2 (T) [mm]	0,3	1,7	6	8	9	10
Strut [mm]	0	0	0	4	5	6



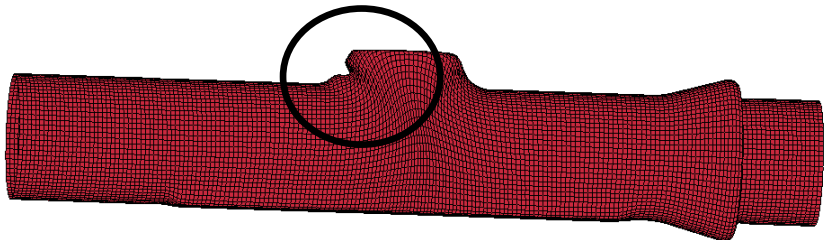
Sample 44	Simulation	Reality
(Strut-)Height	64,74	70,56 (~38,9 %)
Length	307,26	319
Failure	No	No

Component failure when considering anisotropy

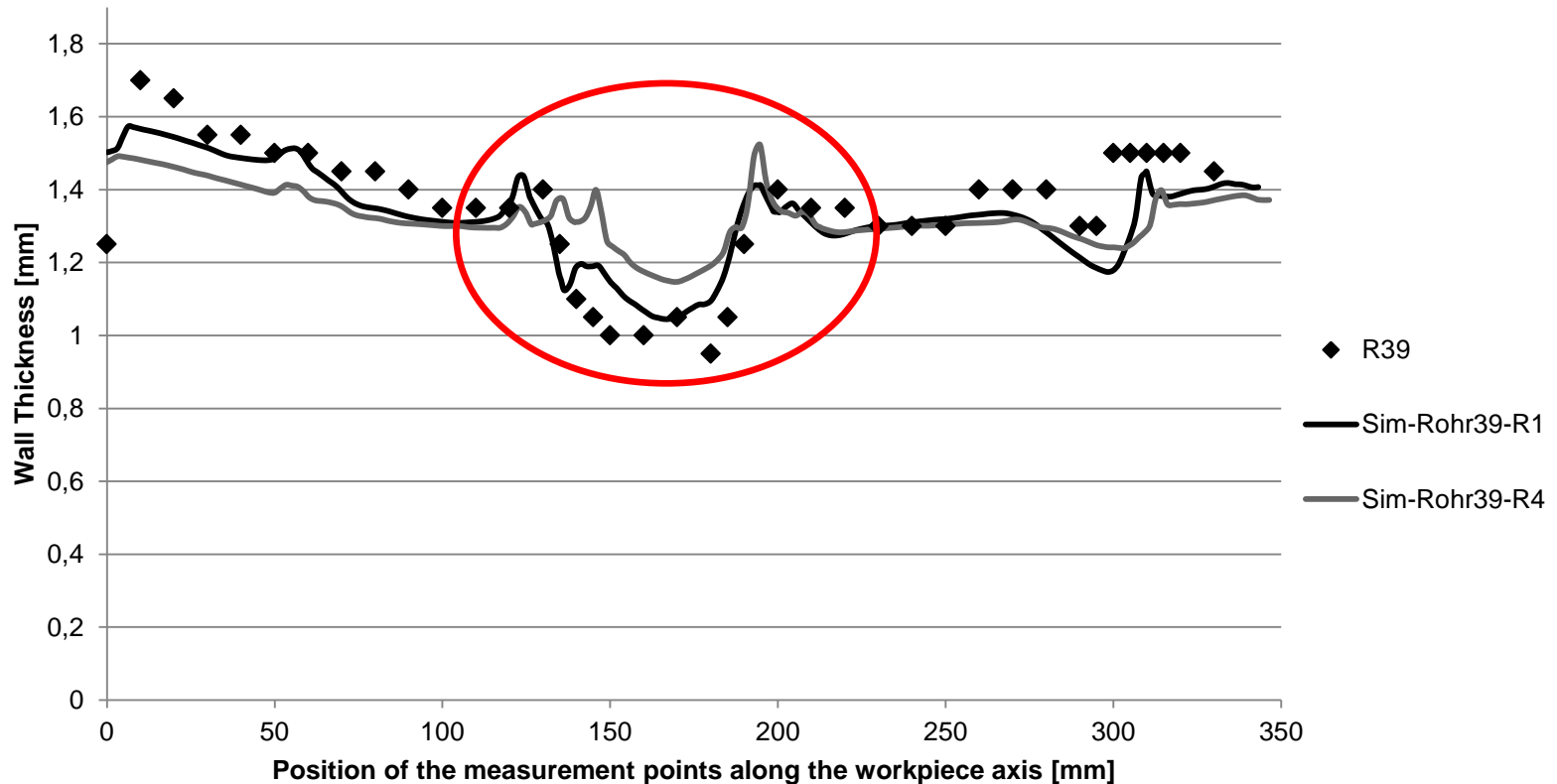
Boundary conditions	
Element type	16
Material Model	037 Transversely Anisotropy
Anisotropy	1



Boundary conditions	
Element type	16
Material Model	037 Transversely Anisotropy
Anisotropy	4



Wall thickness distribution in its dependencies of the anisotropy



Abstract

- Basic studies on hydroforming of titanium alloys have been successfully completed
- Multi-stage process chain has been successfully designed for shaping titanium tubes
- Demonstration parts have been successfully created

Forecast

- Improving the simulation results
- Defining an universal range of parameters

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